# SIMULATION OF Si AND SiO<sub>2</sub> ETCHING IN CF<sub>4</sub> + H<sub>2</sub> PLASMA

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The reactive ion etching of silicon and silicon oxide in  $CF_4+H_2$  plasma is considered by the proposed model, which includes processes of adsorption, chemical reactions, desorption, sputtering, and stochastic mixing. The etching rates are calculated as functions of concentrations of chemically active and inactive plasma components and ion bombardment parameters. The chemical composition of  $CF_4 + H_2$  plasma is calculated to achieve the goal. It is found that the reaction products and  $CF_2$ radicals cover the silicon surface.  $CF_2$  radicals penetrate in the bulk and form an altered layer in the near-surface region. At high  $H_2$  content in the feed (>30%), the deposition of fluorocarbon polymer takes place. Meanwhile, the concentrations of adsorbed layer components are low during SiO<sub>2</sub> etching in  $CF_4 + H_2$  plasma.

Keywords:  $CF_4 + H_2$  plasma, Si, SiO<sub>2</sub>, reactive ion etching

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# 1. Introduction

Selective etching of silicon oxide over silicon or silicon nitride in fluorocarbon plasmas is widely used in integrated circuit manufacture. Fluorocarbon plasmas produce  $CF_x$  ( $x \le 3$ ) radicals that polymerize on surfaces in contact with the plasma. Oxygen from the SiO<sub>2</sub> surface, aided by ion bombardment, prevents the build-up of polymer and allows net etching. The lack of oxygen, on the other hand, permits polymer deposition on the silicon surface and promotes selectivity [1–3].

The fluorocarbon layer is formed on both  $SiO_2$  and Si surfaces during etching in  $CF_4 + H_2$  plasma. The thickness of the fluorocarbon layer on SiO<sub>2</sub> is much smaller than on Si for comparable discharge conditions [4, 5]. During Si etching in  $CF_4 + H_2$  plasma the adsorption of CF<sub>2</sub> radicals on the Si surface is enhanced by ion bombardment, i.e. the sticking coefficient of CF<sub>2</sub> radicals on the Si surface is increased in the presence of ion bombardment [6]. Meanwhile, the fluorocarbon film is thin on the SiO<sub>2</sub> surface as adsorbed  $CF_x$  ( $x \leq 3$ ) radicals react with surface oxygen to form volatile CO, CO<sub>2</sub>, and COF<sub>2</sub> molecules. These phenomena are used in the selective etching of  $SiO_2$  layers on a Si surface. As the  $SiO_2$  layer is etched, the underlying Si is etched slowly. In this way, the fixed depth trenches and contact holes are formed.

In this work, the main reactions occurring in  $CF_4 + H_2$  plasma are considered and the concentrations of plasma components are calculated by extrapolation from experimental data. Using the derived composition of the flux of particles from the plasma, reactive ion etching (RIE) of Si and SiO<sub>2</sub> is investigated. It is found that CF<sub>2</sub> radicals penetrate in silicon bulk and form an altered layer in the near-surface region. Low SiO<sub>2</sub> surface coverage by the reaction products and CF<sub>2</sub> radicals is confirmed.

# 2. Modelling of Si and SiO<sub>2</sub> etching in $CF_4 + H_2$ plasma

# 2.1. Modelling of chemical composition of $CF_4 + H_2$ plasma

The chemical composition of  $CF_4 + H_2$  plasma is considered. Specific reactions in  $CF_4 + H_2$  plasma are reactions of  $CF_x$  ( $x \le 3$ ) radicals with H atoms [7–9]. In order to reduce the number of frequency probabilities only the main reactions are included in the model:

$$CF_4 + e \rightarrow CF_3 + F + e,$$
 (1.1)

$$H_2 + e \rightarrow 2H + e, \qquad (1.2)$$

$$F + H_2 \rightarrow HF + H, \tag{1.3}$$

$$CF_3 + F + M \rightarrow CF_4 + M,$$
 (1.4)

$$CF_3 + H \rightarrow CF_2 + HF,$$
 (1.5)

$$\mathrm{H} + \mathrm{F} + \mathrm{M} \mathop{\rightarrow} \mathrm{HF} + \mathrm{M}, \tag{1.6}$$

$$2H + M \rightarrow H_2 + M. \tag{1.7}$$

Reaction rates are characterized by frequency probabilities of dissociation  $G_i$  and reaction  $R_{ij}$ :

$$G_1 = \frac{g_1[\mathbf{e}]}{N},\tag{2.1}$$

$$G_2 = \frac{g_2[\mathbf{e}]}{N},$$
 (2.2)

$$R_{25} = k_3, \tag{2.3}$$

$$R_{35} = \frac{k_4[M]}{N},$$
 (2.4)

$$R_{36} = k_5, \tag{2.5}$$

$$R_{56} = \frac{k_6[M]}{N},$$
 (2.6)

$$R_{66} = \frac{k_7[M]}{N},$$
 (2.7)

where  $g_i$  is the dissociation rate constant of the *i*th reaction, N is the total neutral particle concentration in the plasma,  $k_i$  is the reaction rate constant of the *i*th reaction, and M is a third particle or the wall of the reactor. Let us assume that frequency probabilities of dissociation and reaction do not depend on H<sub>2</sub> content in the feed.

It follows that seven chemical species exist in the plasma: CF<sub>4</sub>, H<sub>2</sub>, CF<sub>3</sub>, CF<sub>2</sub>, F, H, and HF, with relative concentrations  $n_1 = [CF_4]/N$ ,  $n_2 = [H_2]/N$ ,  $n_3 = [CF_3]/N$ ,  $n_4 = [CF_2]/N$ ,  $n_5 = [F]/N$ ,  $n_6 = [H]/N$ , and  $n_7 = [HF]/N$ , respectively. The following system of rate equations describes the kinetics of chemical composition of CF<sub>4</sub> + H<sub>2</sub> plasma:

$$\frac{\mathrm{d}n_1}{\mathrm{d}t} = I_1 - G_1 n_1 + R_{35} n_3 n_5 - E n_1, \tag{3.1}$$

$$\frac{\mathrm{d}n_2}{\mathrm{d}t} = I_2 - G_2 n_2 - R_{25} n_2 n_5 + R_{66} n_6^2 - E n_2, \ (3.2)$$

$$\frac{\mathrm{d}n_3}{\mathrm{d}t} = G_1 n_1 - R_{35} n_3 n_5 - R_{36} n_3 n_6 - E n_3, \quad (3.3)$$

$$\frac{\mathrm{d}n_4}{\mathrm{d}t} = R_{36}n_3n_6 - En_4,\tag{3.4}$$

$$\frac{m_5}{dt} = G_1 n_1 - R_{25} n_2 n_5 - R_{35} n_3 n_5 - R_{56} n_5 n_6 - E n_5,$$
(3.5)

$$\frac{\mathrm{d}n_6}{\mathrm{d}t} = 2G_2n_2 + R_{25}n_2n_5 - R_{36}n_3n_6 - R_{56}n_5n_6 - 2R_{66}n_6^2 - En_6,$$
(3.6)

$$\frac{\mathrm{d}n_7}{\mathrm{d}t} = R_{25}n_2n_5 + R_{36}n_3n_6 + R_{56}n_5n_6 - En_7,$$
(3.7)

where  $I_i = \Phi_i/(V_0N)$  is the injection rate of the *i*th component of gas mixture, *E* is the frequency probability of exhaust,  $\Phi_i$  is the flow rate of the *i*th component, and  $V_0$  is the volume of the reactor.

#### 2.2. Modelling of Si etching

The RIE of a Si substrate in  $CF_4 + H_2$  plasma is considered. The relative concentrations of plasma components calculated from the previous model of plasma composition are used for the calculation of the etching rates. The main reactions taking place on the surface are the following:

$$Si + 4F \rightarrow SiF_4,$$
 (4.1)

$$2\mathrm{Si} + 2\mathrm{CF}_3 \rightarrow \mathrm{SiF}_4 + \mathrm{SiF}_2 + 2\mathrm{C}, \qquad (4.2)$$

$$\operatorname{Si} + 2\operatorname{CF}_2 \to \operatorname{SiF}_4 + 2\operatorname{C},$$
 (4.3)

$$\operatorname{Si} + \operatorname{CF}_2 \to \operatorname{Si} - \operatorname{CF}_2,$$
 (4.4)

$$\mathrm{CF}_2(s) + \mathrm{CF}_2 \to \mathrm{CF}_2 - \mathrm{CF}_2(s). \tag{4.5}$$

Reactions (4.1)–(4.3) are characterized by reaction rate constants  $k_1$ ,  $k_2$ , and  $k_3$ , and reactions (4.4) and (4.5) by sticking coefficients  $\alpha_{43}$  and  $\alpha_{44}$ . The relative flux of *i*th type plasma species to the surface is equal to  $S_{i,0} = J_{i,0}/C$ , where  $J_{i,0} = n_i N [kT/(2\pi m_i)]^{1/2}$  is the flux of *i*th type species, k is the Boltzmann constant, T is temperature,  $m_i$  is the mass of *i*th type species, and  $C = 1.36 \cdot 10^{19} \text{ m}^{-2}$  is the concentration of surface atoms. Let us assume that C atoms produced during reactions (4.2) and (4.3) do not stick on the surface or form clusters that occupy small surface area [10]. The reaction products desorb and are sputtered by incident ions. The frequency probability of removal of *i*th adsorbed layer component  $\omega_i$  consists of frequency probabilities of desorption and sputtering:

$$\omega_{i} = \omega_{i,d} + \omega_{i,s}$$
$$= \nu_{0} \exp\left(-\frac{E_{i,d}}{kT}\right) + \frac{Y_{i}I_{0}}{C},$$
(5)

where  $\nu_0$  is the frequency of oscillation of atoms in the solid, and  $E_{i,d}$  is the desorption activation energy of *i*th type molecules,  $Y_i$  is the sputtering yield of the *i*th component,  $I_0$  is the ion flux. Let us assume that ions have the same energy and strike the surface perpendicularly. As the processes of adsorption and removal take place simultaneously, the stochastic mixing between monolayers (ML) occurs. When a particle is adsorbed on the surface, a particle of kth monolayer is transferred into (k + 1)th monolayer, and when a particle is removed from the surface, a particle of kth monolayer is transferred into (k - 1)th monolayer.

Chemically neutral components produced during reactions on the surface are included in the adsorbed layer of one-monolayer thickness. It follows that two components exist in the adsorbed layer: SiF<sub>2</sub> and SiF<sub>4</sub>, with relative concentrations  $c_1 = [SiF_2]/C$  and  $c_2 = [SiF_4]/C$ ; two components exist on the surface: Si and CF<sub>2</sub>, with relative concentrations  $c_3 = [Si]/C$  and  $c_4 = [CF_2]/C$ . The relative concentrations of surface components must fulfill the condition  $c_1 + c_2 = 1$ . The following system of equations includes rate expressions of different processes [11, 12] and describes the kinetics of component concentrations in the adsorbed layer and in the near-surface region:

$$\frac{\mathrm{d}c_1}{\mathrm{d}t} = \frac{k_2 \beta c_3^{(1)} n_3}{2} - \omega_1 c_1, \tag{6.1}$$

$$\frac{\mathrm{d}c_2}{\mathrm{d}t} = k_1 \beta c_3^{(1)} n_5^4 + \frac{k_2 \beta c_3^{(1)} n_3}{2} + k_3 \beta c_3^{(1)} n_4^2 - \omega_2 c_2, \qquad (6.2)$$

$$\frac{\mathrm{d}c_3^{(1)}}{\mathrm{d}t} = \omega_4 c_3^{(2)} - \alpha_{43} \beta c_3^{(1)} n_4, \tag{6.3}$$

$$\frac{\mathrm{d}c_3^{(k)}}{\mathrm{d}t} = -(V_\mathrm{A} + V_\mathrm{S})c_3^{(k)} + V_\mathrm{A}c_3^{(k-1)} + V_\mathrm{S}c_3^{(k+1)}, \quad k \ge 2, \tag{6.4}$$

where  $\beta = 1 - \Theta$  is the fraction of the surface not covered with adsorbate,  $\Theta = \sum_{i=1}^{4} c_i$  is the surface coverage, and  $n_i$  is the relative concentration of the *i*th plasma component,  $V_A = \alpha_{43}c_3^{(1)}n_4 + \alpha_{44}c_4^{(1)}n_4$  is the adsorption rate, and  $V_S = \omega_1c_1 + \omega_2c_2 + \omega_4c_4^{(1)}$  is the removal rate. The etching rate V is proportional to the difference of removal and adsorption rates:

$$V = h_0 (V_{\rm S} - V_{\rm A}) \tag{7}$$

where  $h_0 = 2.72$  Å is the monolayer thickness, which is estimated using the expression  $h_0 = [M_{\rm Si}/(\rho_{\rm Si}N_{\rm A})]^{1/3}$ , where  $M_{\rm Si} = 2.809 \cdot 10^{-2}$  kg/mol is the atomic weight of Si,  $\rho_{\rm Si} = 2330$  kg/m<sup>3</sup> is the density of Si, and  $N_{\rm A}$  is Avogadro's number.

## 2.3. Modelling of $SiO_2$ etching

The RIE of a SiO<sub>2</sub> film in  $CF_4 + H_2$  plasma is considered. The relative concentrations of plasma components calculated from the previous model of plasma composition are used for the calculation of the etching rates. The main reactions taking place on the surface are the following:

$$2\operatorname{SiO}_2 + 2\operatorname{CF}_3 \rightarrow \operatorname{SiF}_2 + \operatorname{SiF}_4 + 2\operatorname{CO}_2, \quad (8.1)$$

$$\operatorname{SiO}_2 + 2\operatorname{CF}_2 \to \operatorname{SiF}_4 + 2\operatorname{CO}.$$
 (8.2)

These reactions are characterized by reaction rate constants  $k_1$  and  $k_2$ , respectively. Chemically neutral components produced during reactions on the surface are included in the adsorbed layer of one monolayer thickness. It follows that four components exist in the adsorbed layer: SiF<sub>2</sub>, SiF<sub>4</sub>, CO, and CO<sub>2</sub>, with relative concentrations  $c_1 = [SiF_2]/C$ ,  $c_2 = [SiF_4]/C$ ,  $c_3 = [CO]/C$ , and  $c_4 = [CO_2]/C$ , where  $C = 8.90 \cdot 10^{18} \text{ m}^{-2}$  is the concentration of surface molecules. The following system of equations includes rate expressions of different processes [11, 13] and describes the kinetics of component concentrations in the adsorbed layer:

$$\frac{\mathrm{d}c_1}{\mathrm{d}t} = k_1 \beta n_3^2 - \omega c_1, \qquad (9.1)$$

$$\frac{\mathrm{d}c_2}{\mathrm{d}t} = k_1 \beta n_3^2 + k_2 \beta n_4^2 - \omega c_2, \qquad (9.2)$$

$$\frac{\mathrm{d}c_3}{\mathrm{d}t} = 2k_2\beta n_4^2 - \omega c_3,\tag{9.3}$$

$$\frac{\mathrm{d}c_4}{\mathrm{d}t} = 2k_1\beta n_3^2 - \omega c_4. \tag{9.4}$$

The surface concentrations of components under steadystate conditions are equal to

$$c_{1,\text{St}} = \frac{k_1 n_3^2}{4k_1 n_3^2 + 3k_2 n_4^2 + \omega},$$
 (10.1)

$$c_{2,\text{St}} = \frac{k_1 n_3^2 + k_2 n_4^2}{4k_1 n_3^2 + 3k_2 n_4^2 + \omega},$$
 (10.2)

$$c_{3,\text{St}} = \frac{2k_2n_4^2}{4k_1n_3^2 + 3k_2n_4^2 + \omega},$$
 (10.3)

$$c_{4,\text{St}} = \frac{2k_1n_3^2}{4k_1n_3^2 + 3k_2n_4^2 + \omega}.$$
 (10.4)

The etching rate is proportional to the removal rate of formed  $SiF_2$  and  $SiF_4$  molecules. According to Eqs. (10.1) and (10.2) the etching rate under steady-state conditions is equal to

$$V_{\rm St} = \frac{h_0 \omega (2k_1 n_3^2 + k_2 n_4^2)}{4k_1 n_3^2 + 3k_2 n_4^2 + \omega},\tag{11}$$

where  $h_0 = 3.35$  Å is the monolayer thickness.

# 3. Results and discussion

# 3.1. Chemical composition of $CF_4 + H_2$ plasma

The experimentally measured dependences of relative concentrations of H<sub>2</sub> and HF molecules in CF<sub>4</sub> + H<sub>2</sub> plasma on H<sub>2</sub> content in the feed [7] are used for calculating the chemical composition of CF<sub>4</sub> + H<sub>2</sub> plasma. This experiment is chosen because of mass spectrometry measurements of plasma composition. It is assumed that the flow rate of gas mixture is 30 sccm, the pressure is 133 Pa, the reactor volume is  $1.3 \cdot 10^{-4}$  m<sup>-3</sup>, and the plasma temperature is 500 K. The total gas injection rate of 5.47 s<sup>-1</sup> is estimated using the expression  $I = \Phi/(V_0N)$ , where  $N = 1.93 \cdot 10^{22}$  m<sup>-3</sup> is the total neutral particle concentration, and the flow rate  $\Phi$  is measured in molecules/s.

Experimental [7] and theoretical dependences of the relative concentration of H<sub>2</sub> and HF molecules in the plasma on H<sub>2</sub> content in the feed calculated using Eq. (3) under steady-state conditions are shown in Fig. 1. The following values of frequency probabilities of dissociation and reaction are used:  $G_1 = 3.7 \text{ s}^{-1}$ ,  $G_2 = 2.0 \text{ s}^{-1}$ ,  $R_{25} = 1.0 \cdot 10^4 \text{ s}^{-1}$ ,  $R_{35} = 100 \text{ s}^{-1}$ ,  $R_{36} = 2.0 \cdot 10^4 \text{ s}^{-1}$ ,  $R_{56} = 1.0 \cdot 10^4 \text{ s}^{-1}$ ,  $R_{66} = 100 \text{ s}^{-1}$ ,  $E = 5.47 \text{ s}^{-1}$ . These values were determined by extrapolation from experimental results [13, 14].



Fig. 1. Experimental [7] (points) and theoretical (curves) dependences of the relative concentrations of  $H_2$  and HF molecules on  $H_2$  content in the feed.



Fig. 2. The chemical composition of  $CF_4 + H_2$  plasma as a function of  $H_2$  content in the feed.

The chemical composition of  $CF_4 + H_2$  plasma as a function of H<sub>2</sub> content in the feed calculated using Eq. (3) under steady-state conditions is shown in Fig. 2. The concentration of HF molecules with increase of H<sub>2</sub> content in the feed increases at first due to the reactions of H atoms with F atoms and  $CF_3$  radicals (Eqs. (1.5) and (1.6)). As the concentration of HF molecules approaches the maximum value, almost all F atoms and CF<sub>3</sub> radicals have reacted (Fig. 2). With further increase in H<sub>2</sub> content in the feed the concentration of HF molecules starts to decrease in proportion to the amount of injected CF<sub>4</sub> molecules. At H<sub>2</sub> content in the plasma >30%, the concentration of CF<sub>2</sub> radicals is about 10 times higher than that of  $CF_3$  (Fig. 2) or CF radicals [8,9]. This indicates that the reaction of H atoms with CF<sub>3</sub> radicals is intensive. Due to intensive



Fig. 3. The dependence of pressure on H<sub>2</sub> content in the feed.



Fig. 4. The dependences of the conversion coefficients of  $CF_4$  and  $H_2$  molecules on  $H_2$  content in the feed.

reactions taking place in  $CF_4 + H_2$  plasma the pressure in the reactor increases (Fig. 3).

The conversion coefficient of the ith component of the gas mixture indicates the part of molecules converted to reaction products and is equal to

$$\eta_i = 1 - \frac{En_i}{I_i}.$$
(12)

The dependences of the conversion coefficients of  $CF_4$  and  $H_2$  molecules on  $H_2$  content in the feed are presented in Fig. 4. At  $H_2$  content in the feed <30%, all  $H_2$  molecules are converted to reaction products. The conversion coefficient of  $CF_4$  molecules increases due to the dissociation reaction (1.1) and subsequent reaction (1.5) of H atoms with  $CF_3$  radicals. At high  $H_2$  content the conversion coefficient of  $CF_4$  molecules is constant, and conversion of  $H_2$  molecules decreases due to dilution of  $CF_4$  gas.



Fig. 5. Experimental [15] (points) and theoretical (curves) dependences of RIE rates of Si and  $SiO_2$  on  $H_2$  content in the feed.

#### 3.2. Si etching

The experimentally measured dependence of the RIE rate of Si on  $H_2$  content in the feed [15] is used in the model in order to calculate etching rates. Let us assume that the Si etching rate in the absence of  $H_2$  in the feed is equal to a value measured during experiment [16]. Experimental [15] and theoretical dependences of RIE rates of Si on  $H_2$  content in the feed calculated using Eq. (7) are shown in Fig. 5. The following values of reaction rate constants, sticking coefficients, and frequency probabilities of removal are found by extrapolation:  $k_1 = 5.0 \cdot 10^7 \text{ s}^{-1}, k_2 = 8.0 \cdot 10^4 \text{ s}^{-1},$  $k_3 = 5.0 \cdot 10^4 \text{ s}^{-1}, \ \alpha_{43} = 39 \text{ s}^{-1}, \ \alpha_{44} = 4.0 \cdot 10^4 \text{ s}^{-1}, \ \omega_1 = \omega_2 = 1200 \text{ s}^{-1}, \ \omega_4 = 14 \text{ s}^{-1}.$  The etching rate approaches the steady-state regime within 1 s. It is important to note that the sticking coefficient of CF<sub>2</sub> radicals from the plasma on CF2 radicals on the surface is three orders higher than on Si atoms. Due to preferential sticking the concentration of CF<sub>2</sub> radicals on the surface is low (Fig. 6), and the etched surface is rough. The obtained results are in agreement with the experimental measurements [17].

The dependences of the concentrations of adsorbed layer components on  $H_2$  content in the feed are shown in Fig. 6. The minimum is observed in the dependence of concentration of SiF<sub>4</sub> molecules on  $H_2$  content in the feed. It is a result of simultaneous formation of SiF<sub>2</sub> and SiF<sub>4</sub> molecules (Eq. (4.2)). Concentrations of CF<sub>2</sub> radicals in the near-surface region at different  $H_2$  content in the feed are shown in Fig. 7. It is observed that the thickness of the altered layer increases with the increase of  $H_2$  content in the feed due to increased flux of CF<sub>2</sub> radicals to the surface. The concentration of



Fig. 6. The dependences of the concentrations of adsorbed layer components on  $H_2$  content in the feed during RIE of silicon in  $CF_4 + H_2$  plasma.



Fig. 7. Concentrations of  $CF_2$  radicals in the near-surface region at different  $H_2$  content in the feed.

 $CF_2$  radicals in the near-surface region does not change during the deposition of the fluorocarbon film.

#### 3.3. $SiO_2$ etching

The experimentally measured dependence of the RIE rate of SiO<sub>2</sub> on H<sub>2</sub> content in the feed [15] is used in the model in order to calculate etching rates. Let us assume that the SiO<sub>2</sub> etching rate in the absence of H<sub>2</sub> in the feed is equal to a value measured during experiment [16]. Experimental and theoretical dependences of RIE rates of SiO<sub>2</sub> on H<sub>2</sub> content in the feed calculated using Eq. (11) are shown in Fig. 5. The following values of reaction rate constants and frequency probability of removal are used:  $k_1 = 19 \text{ s}^{-1}$ ,  $k_2 = 14 \text{ s}^{-1}$ ,  $\omega = 10 \text{ s}^{-1}$ . These values were determined by extrapolation from experimental results [13].



Fig. 8. The dependences of the concentrations of adsorbed layer components on  $H_2$  content in the feed during RIE of SiO<sub>2</sub> in  $CF_4 + H_2$  plasma.

The dependences of the concentrations of adsorbed layer components on  $H_2$  content in the feed are shown in Fig. 8. It is observed that the concentrations of adsorbed layer components are low. The dependences of concentrations of  $CO_2$  and  $SiF_2$  molecules are similar to the dependence of the concentration of  $CF_3$  radicals in the plasma. It is influenced by the same reaction of  $CF_3$  radicals with  $SiO_2$  molecules (Eq. (8.1)). The maxima of the concentrations of CO and  $SiF_4$  molecules are achieved at the maximum concentration of  $CF_2$  radicals in the plasma. The obtained results are in agreement with the experimental measurements [6, 18].

#### 4. Conclusions

1. In  $CF_4 + H_2$  plasma at  $H_2$  content in the feed <30%, all  $H_2$  molecules are converted to reaction products. It is a result of intensive dissociation and subsequent reaction of H atoms with  $CF_3$  radicals.

2. During RIE of Si in  $CF_4 + H_2$  plasma  $CF_2$  radicals penetrate in the bulk and form an altered layer in the near-surface region. The thickness of the altered layer increases with the increase of  $H_2$  content in the feed due to increased flux of  $CF_2$  radicals to the surface.

3. During RIE of SiO<sub>2</sub> in  $CF_4 + H_2$  plasma the concentrations of adsorbed layer components are low.

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# Si IR SiO<sub>2</sub> ÉSDINIMO $CF_4 + H_2$ PLAZMOJE MODELIAVIMAS

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#### Santrauka

Išnagrinėtas silicio ir silicio oksido reaktyvus joninis ėsdinimas  $CF_4 + H_2$  plazmoje. Pasiūlytame modelyje atsižvelgta į įgerties, cheminių reakcijų, atvirkštinės gerties, dulkėjimo ir stochastinio maišymo vyksmus. Esdinimo spartos vertės apskaičiuotos kaip chemiškai aktyvių ir neaktyvių plazmos sandų koncentracijų bei joninio apšaudymo parametrų funkcija. Tikslui pasiekti apskaičiuota

 $CF_4 + H_2$  plazmos cheminė sudėtis. Rasta, kad reakcijos produktai ir  $CF_2$  radikalai dengia silicio paviršių.  $CF_2$  radikalai prasiskverbia į tūrį ir sudaro pakeistą sluoksnį. Esant dideliam  $H_2$  kiekiui įleidžiamame mišinyje (>30%), susidaro fluorokarboninis polimeras. Tačiau silicio oksido ėsdinimo  $CF_4 + H_2$  plazmoje metu įgerto sluoksnio sandų koncentracijos yra mažos.